Self-consistent calculation of metamaterials with gain

A. Fang,1 Th. Koschny,1,2 M. Wegener,3 and C. M. Soukoulis1,2

1Department of Physics and Astronomy and Ames Laboratory, Iowa State University, Ames, Iowa 50011, USA
2Department of Materials Science and Technology and Institute of Electronic Structure and Laser, FORTH, University of Crete, 71110 Heraklion, Crete, Greece
3Institut für Angewandte Physik and DFG-Center for Functional Nanostructures (CFN), Universität Karlsruhe (TH), D-76128 Karlsruhe, Germany

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We present a computational scheme allowing for a self-consistent treatment of a dispersive metallic photonic metamaterial coupled to a gain material incorporated into the nanostructure. The gain is described by a generic four-level system. A critical pumping rate exists for compensating the loss of the metamaterial. Nonlinearities arise due to gain depletion beyond a certain critical strength of a test field. Transmission, reflection, and absorption data as well as the retrieved effective parameters are presented for a lattice of resonant square cylinders embedded in layers of gain material and split ring resonators with gain material embedded into the gaps.

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The field of metamaterials,1,2 is driven by fascinating and far-reaching theoretical visions such as, e.g., perfect lenses,3 invisibility cloaking,4,5 and enhanced optical nonlinearities.6 This emerging field has seen spectacular experimental progress in recent years.1,2 Yet, losses are orders of magnitude too large for the envisioned applications. Achieving such reduction by further design optimization appears to be out of reach. Thus, incorporation of active media (gain) might come as a cure. The dream would be to simply inject an electrical current into the active medium, leading to gain and hence to compensation of the losses. However, experiments on such intricate active nanostructures do need guidance by theory via self-consistent calculations (using the semiclassical theory of lasing) for realistic gain materials that can be incorporated into or close to dispersive media to reduce the losses at THz or optical frequencies. The need for self-consistent calculations stems from the fact that increasing the gain in the metamaterial, the metamaterial properties change, in turn changes the coupling to the gain medium until a steady state is reached. A specific geometry to overcome the severe loss problem of optical metamaterials and to enable bulk metamaterials with negative magnetic and electric responses and controllable dispersion at optical frequencies is to interleave active optically pumped gain material layers with the passive metamaterial lattice.

For reference, the best fabricated negative-index material operating at around 1.4 μm wavelength7 has shown a figure of merit (FOM)=−Re(n)/Im(n)≈3, where n is the effective refractive index. This experimental result is equivalent to an absolute absorption coefficient of α=3×10^4 cm⁻¹, which is even larger than the absorption of typical direct-gap semiconductors such as, e.g., GaAs (where α=10^4 cm⁻¹). So it looks difficult to compensate the losses with this simple type of analysis, which assumes that the bulk gain coefficient is needed. However, the effective gain coefficient, derived from self-consistent microscopic calculations, is a more appropriate measure of the combined system of metamaterial and gain. Due to pronounced local-field enhancement effects in the spatial vicinity of the dispersive metamaterial, the effective gain coefficient can be substantially larger than its bulk counterpart. While early models using simplified gain mechanisms such as explicitly forcing negative imaginary parts of the local gain material’s response function produce unrealistic strictly linear gain, our self-consistent approach presented below allows for determining the range of parameters for which one can realistically expect linear amplification and linear loss compensation in the metamaterial. To fully understand the coupled metamaterial-gain system, we have to deal with time-dependent wave equations in metamaterial systems by coupling the Maxwell equations with the rate equations of electron populations describing a multilevel gain system in semiclassical theory.8

In this Rapid Communication, we apply a detailed computational model to the problem of metamaterials with gain. The generic four-level atomic system tracks fields and occupation numbers at each point in space, taking into account energy exchange between atoms and fields, electronic pumping and nonradiative decays.8 An external mechanism pumps electrons from the ground-state level N₀ to the third level N₃ at a certain pumping rate Γₚump, which is proportional to the optical pumping intensity in an experiment. After a short lifetime τ₋₂ electrons transfer nonradiatively into the metastable second level N₂. The second level (N₂) and the first level (N₁) are called the upper and lower lasing levels. Electrons can be transferred from the upper to the lower lasing level by spontaneous and stimulated emission. At last, electrons transfer quickly and nonradiatively from the first level (N₁) to the ground-state level (N₀). The lifetimes and energies of the upper and lower lasing levels are τ₋₂, E₂ and τ₋₁, E₁, respectively. The center frequency of the radiation is ω₀=(E₂−E₁)/ħ which is chosen to be equal to 2π×10¹⁴ Hz. The parameters τ₋₂, τ₋₁ and τ₋₀ are chosen to be 5×10⁻¹⁴, 5×10⁻¹², and 5×10⁻¹⁴ s, respectively. The total electron density, Nₓ(t=0) = N₀(t)+N₁(t)+N₂(t)+N₃(t)=5.0×10²³/m³, and the pump rate Γₚump are controlled variables according to the experiment. The time-dependent Maxwell equations are given by ∇×E=−∂B/∂t and ∇×H=ε₀εₔE/ε₀+μ₀μₔP/ε₀, where B=μ₀μₔH and P is the dispersive electric polarization density from which the amplification and gain can be obtained. Following the single-electron case, we can show8 that the polarization density P(r,t) in the presence of an electric...
chosen to be FDTD calculations, the discrete time and space steps are according to the system of equations above.

\[
\frac{\partial^2 \mathbf{P}(t)}{\partial t^2} + \Gamma_a \frac{\partial \mathbf{P}(t)}{\partial t} + \omega_c^2 \mathbf{P}(t) = -\sigma_a \Delta N(i,t) \mathbf{E}(t),
\]

where \( \Gamma_a \) is the linewidth of the atomic transition \( \omega_a \) and is equal to \( 2\pi \times 5 \times 10^{12} \) Hz or \( 2\pi \times 20 \times 10^{12} \) Hz. The factor \( \Delta N(r,t) = N_S - N_L = \Delta N(r,t) \) is the population inversion that drives the polarization and \( \sigma_a \) is the coupling strength of \( \mathbf{P} \) to the external electric field and its value is taken to be \( 10^{-9} \) C²/kg. It follows\(^8\) from Eq. (1) that the amplification line shape is Lorentzian and homogeneously broadened.\(^9\)

The occupations numbers at each spatial point vary according to

\[
\frac{\partial N_3}{\partial t} = \Gamma_{\text{pump}} N_0 - \frac{N_3}{\tau_{32}},
\]

\[
\frac{\partial N_2}{\partial t} = \frac{N_3}{\tau_{32}} + \frac{1}{\hbar \omega_a} \mathbf{E} \cdot \frac{\partial \mathbf{P}}{\partial t} - \frac{N_2}{\tau_{21}},
\]

\[
\frac{\partial N_1}{\partial t} = \frac{N_2}{\tau_{21}} + \frac{1}{\hbar \omega_a} \mathbf{E} \cdot \frac{\partial \mathbf{P}}{\partial t} - \frac{N_1}{\tau_{10}},
\]

\[
\frac{\partial N_0}{\partial t} = \frac{N_1}{\tau_{10}} - \Gamma_{\text{pump}} N_0,
\]

where \( \frac{1}{\hbar \omega_a} \mathbf{E} \cdot \frac{\partial \mathbf{P}}{\partial t} \) is the induced radiation rate or excitation rate depending on its sign.

In order to solve the behavior of the active materials in the electromagnetic fields numerically, the finite-difference time-domain (FDTD) technique is utilized,\(^10\) using an approach similar to the one outlined in Refs. \(10, 12\). In the FDTD calculations, the discrete time and space steps are chosen to be \( \Delta t = 8.33 \times 10^{-18} \) s and \( \Delta x = 5.0 \times 10^{-9} \) m for simulations on the structure as shown in Fig. 1, and \( \Delta t = 8.33 \times 10^{-19} \) s and \( \Delta x = 1.0 \times 10^{-9} \) m for simulations on the structure as shown in Fig. 5. The initial condition is that all the electrons are in the ground state, so there is no field, no polarization, and no spontaneous emission. Then the electrons are pumped from \( N_0 \) to \( N_3 \) (then relaxing to \( N_2 \)) with a constant pumping rate \( \Gamma_{\text{pump}} \). The system begins to evolve according to the system of equations above.

We have performed numerical simulations on one-dimensional and two-dimensional (2D) systems with gain.\(^13\) Previous studies\(^14-18\) have considered loss reduction by incorporating gain but where not self-consistent (see the introduction).\(^14-17\) As the first simple model system, we will discuss a 2D metamaterial system (shown in Fig. 1) which consists of layers of gain material and dielectric wires that have a resonant Lorentz-type electric response to emulate the resonant elements in a realistic metamaterial. We will have to study whether we will be able to compensate the losses of the metamaterials associated with the Lorentz resonance in the wires by the amplification provided by the gain material layers without destroying the linear response of the metamaterial. First we generate a narrow-band Gaussian pulse of a given amplitude and let it propagate through the metamaterial without gain, and we calculate the transmitted signal emerging from the metamaterial which has also Gaussian profile but the amplitude is much smaller than that of the incident pulse depending on how much loss occurs in the metamaterial. Then we introduce the gain and start increasing the pumping rate and find a critical pumping rate, \( \Gamma_{\text{pump}} \approx 2.65 \times 10^9 \) s⁻¹, for which the transmitted pulse is of the same amplitude as the incident pulse. In addition, for fixed pumping rate, we start increasing the amplitude of the incident Gaussian pulse and we would like to see how high we can go in the strength of the incident electric field and still have full compensation of the losses, i.e., the transmitted signal equals the incident signal, independent on the signal strength. In this region we have compensated loss and still linear response of the metamaterial; here, the shape of the transmitted Gaussian is only affected by the dispersion but not dependent on the signal strength.

We have calculated the transmission versus the strength of the electric field of the incident signal for several pumping rates close to the critical pumping rate. As shown in Fig. 2, we found that for a rather broad region of low intensity input signal we have a linear response all the way up to incident electric field of \( 10^3 \) V/m. If we use only three layers (rods-gain material-rods), the critical pumping rate is \( 4.85 \times 10^9 \) s⁻¹, which is two times higher than the 19-layer case of Fig. 1. In Fig. 3, we present detailed results for the
The critical pumping rate versus the number of layers of the system shown in Fig. 1. Notice that, as the number of layers increases, the critical $\Gamma_{\text{pump}}$ decreases. The linear regime for three layers exists up to $10^3$ V/m, and for higher strength drops slower than that of Fig. 2. In all the following simulations, the strength of the incident signal is chosen to be 10 V/m, which is far away from $10^3$ V/m, so we operate in the linear regime of the metamaterial. As an example, we have studied three layers, rods-gain material-rods, to see how the critical pumping rate versus the number of layers of the system in Fig. 1. Parameters for gain and loss are approximately independent. The behavior would obviously be different in a 3D situation, which, however, is computationally excessively demanding. Thus, we consider a 2D version of the split ring resonator (SRR) as a more realistic and also more relevant model. Here, the relevant polarization is across the finite SRR gap and, therefore, the coupling to the gain material is in fact dipolelike.

In Fig. 5, we present the unit cell of our SRR system with gain material embedded in the SRR gap. The dimensions of the SRR are chosen such that a magnetic resonance frequency at 100 THz results, which can overlap with the peak of the emission of the gain material. The FWHM of the gain material is 20 THz and $\Gamma_{\text{pump}}$ is $1.4 \times 10^9$ s$^{-1}$. Simulations are done for one layer of the square SRR. In Fig. 6(a), we plot the retrieved results of the real and the imaginary parts of the magnetic permeability $\mu$, with and without gain. With the introduction of gain, the weak and broad resonant effective $\mu$ (FWHM=5.85 THz) of the lossy SRR becomes strong and narrow (FWHM=1.66 THz); the gain effectively undamps the LCR resonance of the SRR. Notice that here losses in the magnetic effective response are compensated by electric gain in the SRR gap. So with the introduction of gain, we obtain a negative $\mu$ with a very small imaginary part in an otherwise typical SRR response, which means that the losses have been compensated by the gain. In Fig. 6(b), we plot the retrieved results for the effective index of refraction $n$, with and without gain. Note that for a lossless SRR $n$ is purely real away from the resonance and imaginary in a small band above the resonance where $\mu$ is negative. Comparing Re($n$) slightly below the resonance at 97 THz, we find an effective extinction coefficient $\alpha=(\omega/c)\text{Im}(n)\approx 3.50 \times 10^4$ cm$^{-1}$ without gain and $\alpha=1.24 \times 10^4$ cm$^{-1}$ with gain, and hence an effective am-

![FIG. 3](image3.png)

**FIG. 3.** (Color online) The critical pumping rates for different numbers of layers of the system in Fig. 1. Parameters for gain and dielectric materials are the same as Fig. 2.

![FIG. 4](image4.png)

**FIG. 4.** (Color online) The retrieved results for the real and the imaginary parts of the effective permittivity $\varepsilon$, with and without gain. In addition, we have plotted Im($\varepsilon_i$) versus frequency. Below compensation, $\tau=0.75$; gain and Lorentz bandwidths are 20 and 5 THz, respectively.

![FIG. 5](image5.png)

**FIG. 5.** (Color online) Geometry for a unit cell of the square SRR system with gain. The gain (shown in orange) is introduced in the gap region of the SRR. The dimensions are $a=100$ nm, $l=80$ nm, $t=5$ nm, $d=4$ nm, and $w=15$ nm.

![FIG. 6](image6.png)
The induced electric field in the gap is around 550 V/m, which is still in the linear regime, and the incident electric field is 10 V/m. Indeed, taking the observed field enhancement factor in the SRR gap of ≈55, the energy per unit cell produced by the gain material inside the gap is ≈18 times larger than for the homogeneous gain medium, which compares very well to the factor of ≈20 between the simulated SRR effective medium and the homogeneous gain medium. If we further increase the pumping rate the magnetic resonance becomes even narrower (0.96 THz for $\Gamma_{\text{pump}}=1.8\times10^4$ s$^{-1}$). When the pumping rate reaches $\Gamma_{\text{pump}}=1.9\times10^3$ s$^{-1}$, Im($\mu$) becomes negative and we have overcompensated at the resonance frequency. By increasing $\Gamma_{\text{pump}}$ even more (≈5×10$^4$ s$^{-1}$) one starts seeing lasing (spawning) in our system (not shown), which is not in the focus of this work. As long as we are in the linear regime, we do not need to have a self-consistent calculation; our results agree very well with the results obtained using the susceptibilities given in Ref. 9. However, the self-consistent calculation is necessary to determine the range of signals for which we can expect approximately linear response and it is needed if we have very strong fields and we are in the nonlinear regime, especially when we want to study lasing.

In conclusion, we have proposed and numerically solved a self-consistent model incorporating gain in 2D dispersive metamaterials. We show numerically that one can compensate the losses of the dispersive metamaterials. There is a relatively wide range of signal amplitudes for which the loss-compensated metamaterial still behaves linearly; at higher amplitudes the response is nonlinear due to the gain. As an example, we have demonstrated that the losses of the magnetic susceptibility $\mu$ of the SRR can be easily compensated by the gain material. The pumping rate needed to compensate the loss is much smaller than the bulk gain. This aspect is due to the strong local-field enhancement inside the SRR gap.

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9 The real and imaginary parts of the gain profile are given by $\psi = \chi + i\chi'$, where $\chi = \chi_0/(1 + \Delta t^2)$ and $\chi' = -\chi_0/(1 + \Delta t^2)$ with $\Delta t = (2\omega_0 - \omega_0)/\Gamma_0$ and $\chi_0 = -\sigma_0 \Delta N/(\epsilon_0 \omega_0 \Gamma_0)$, where $\Delta N = N_2 - N_1$.
13 We first check that a well-defined lasing threshold exists for a gain material slab with a width of 500 nm. The pumping rate for lasing threshold is $1.6\times10^9$ s$^{-1}$, which corresponds to the incident power of 65 W/mm$^2$ and the output power is 4 $\times 10^3$ W/mm$^2$. If the pumping rate is much higher than the lasing threshold, i.e., $3.5\times10^9$ s$^{-1}$, the occupation numbers $N_2$ and $N_1$ oscillate as a function of time and finally saturate to the stable values. For the parameters used, $N_2 = 7.5\times10^{-5}N_0$ and $N_1 = 2.0\times10^{-4}N_0$.
20 The extinction coefficient (amplification coefficient) of the gain material can be calculated from $\alpha = \omega \chi'/(2c\sqrt{\varepsilon})$, given in Chap. 7 of Ref. 8. For the pumping rate $\Gamma_{\text{pump}}=1.4\times10^3$ s$^{-1}$ and $f = 100$ THz, we obtain $\Delta N = 6.9\times10^{-3}N_0$ [$N_1 = N_0(t=0)=5.0\times10^{23}$/m$^3$], and hence $\alpha = -1.50 \times 10^3$ cm$^{-1}$ at the resonance. In our case for 97 THz, we get $\alpha = -1.39 \times 10^9$ cm$^{-1}$.